

19.52. Model: The heat engine follows a closed cycle with process 1 → 2 and process 3 → 4 being isochoric and process 2 → 3 and process 4 → 1 being isobaric. For a monatomic gas, $C_V = \frac{3}{2}R$ and $C_P = \frac{5}{2}R$.

Visualize: Please refer to Figure P19.52.

Solve: (a) The first law of thermodynamics is $Q = \Delta E_{\text{th}} + W_S$. For the isochoric process 1 → 2, $W_{S\ 1 \rightarrow 2} = 0$ J. Thus,

$$\begin{aligned} Q_{1 \rightarrow 2} &= 3750 \text{ J} = \Delta E_{\text{th}} = nC_V \Delta T \\ \Rightarrow \Delta T &= \frac{3750 \text{ J}}{nC_V} = \frac{3750 \text{ J}}{(1.0 \text{ mol})(\frac{3}{2}R)} = \frac{3750 \text{ J}}{(1.0 \text{ mol})(\frac{3}{2})(8.31 \text{ J/mol K})} = 301 \text{ K} \\ \Rightarrow T_2 - T_1 &= 300.8 \text{ K} \Rightarrow T_2 = 300.8 \text{ K} + 300 \text{ K} = 601 \text{ K} \end{aligned}$$

To find volume V_2 ,

$$V_2 = V_1 = \frac{nRT_1}{p_1} = \frac{(1.0 \text{ mol})(8.31 \text{ J/mol K})(300 \text{ K})}{3.0 \times 10^5 \text{ Pa}} = 8.31 \times 10^{-3} \text{ m}^3$$

The pressure p_2 can be obtained from the isochoric condition as follows:

$$\frac{p_2}{T_2} = \frac{p_1}{T_1} \Rightarrow p_2 = \frac{T_2}{T_1} p_1 = \left(\frac{601 \text{ K}}{300 \text{ K}} \right) (3.00 \times 10^5 \text{ Pa}) = 6.01 \times 10^5 \text{ Pa}$$

With the above values of p_2 , V_2 and T_2 , we can now obtain p_3 , V_3 and T_3 . We have

$$\begin{aligned} V_3 &= 2V_2 = 1.662 \times 10^{-2} \text{ m}^3 & p_3 &= p_2 = 6.01 \times 10^5 \text{ Pa} \\ \frac{T_3}{V_3} &= \frac{T_2}{V_2} \Rightarrow T_3 = \frac{V_3}{V_2} T_2 = 2T_2 = 1202 \text{ K} \end{aligned}$$

For the isobaric process 2 → 3,

$$\begin{aligned} Q_{2 \rightarrow 3} &= nC_P \Delta T = (1.0 \text{ mol})(\frac{5}{2}R)(T_3 - T_2) = (1.0 \text{ mol})(\frac{5}{2})(8.31 \text{ J/mol K})(601 \text{ K}) = 12,480 \text{ J} \\ W_{S\ 2 \rightarrow 3} &= p_3(V_3 - V_2) = (6.01 \times 10^5 \text{ Pa})(8.31 \times 10^{-3} \text{ m}^3) = 4990 \text{ J} \\ \Delta E_{\text{th}} &= Q_{2 \rightarrow 3} - W_{S\ 2 \rightarrow 3} = 12,480 \text{ J} - 4990 \text{ J} = 7490 \text{ J} \end{aligned}$$

We are now able to obtain p_4 , V_4 and T_4 . We have

$$\begin{aligned} V_4 &= V_3 = 1.662 \times 10^{-2} \text{ m}^3 & p_4 &= p_1 = 3.00 \times 10^5 \text{ Pa} \\ \frac{T_4}{p_4} &= \frac{T_3}{p_3} \Rightarrow T_4 = \frac{p_4}{p_3} T_3 = \left(\frac{3.00 \times 10^5 \text{ Pa}}{6.01 \times 10^5 \text{ Pa}} \right) (1202 \text{ K}) = 600 \text{ K} \end{aligned}$$

For isochoric process 3 → 4,

$$\begin{aligned} Q_{3 \rightarrow 4} &= nC_V \Delta T = (1.0 \text{ mol})(\frac{3}{2}R)(T_4 - T_3) = (1.0 \text{ mol})(\frac{3}{2})(8.31 \text{ J/mol K})(-602) = -7500 \text{ J} \\ W_{S\ 3 \rightarrow 4} &= 0 \text{ J} \Rightarrow \Delta E_{\text{th}} = Q_{3 \rightarrow 4} - W_{S\ 3 \rightarrow 4} = -7500 \text{ J} \end{aligned}$$

For isobaric process 4 → 1,

$$\begin{aligned} Q_{4 \rightarrow 1} &= nC_P \Delta T = (1.0 \text{ mol})\frac{5}{2}(8.31 \text{ J/mol K})(300 \text{ K} - 600 \text{ K}) = -6230 \text{ J} \\ W_{S\ 4 \rightarrow 1} &= p_4(V_1 - V_4) = (3.00 \times 10^5 \text{ Pa}) \times (8.31 \times 10^{-3} \text{ m}^3 - 1.662 \times 10^{-2} \text{ m}^3) = -2490 \text{ J} \\ \Delta E_{\text{th}} &= Q_{4 \rightarrow 1} - W_{S\ 4 \rightarrow 1} = -6230 \text{ J} - (-2490 \text{ J}) = -3740 \text{ J} \end{aligned}$$

	W_S (J)	Q (J)	ΔE_{th} (J)
1 → 2	0	3750	3750
2 → 3	4990	12,480	7490
3 → 4	0	-7500	-7500
4 → 1	-2490	-6230	-3740
Net	2500	2500	0

(b) The thermal efficiency of this heat engine is

$$\eta = \frac{W_{\text{out}}}{Q_{\text{H}}} = \frac{W_{\text{out}}}{Q_{1 \rightarrow 2} + Q_{2 \rightarrow 3}} = \frac{2500 \text{ J}}{3750 \text{ J} + 12,480 \text{ J}} = 0.154 = 15.4\%$$

Assess: For a closed cycle, as expected, $(W_s)_{\text{net}} = Q_{\text{net}}$ and $(\Delta E_{\text{th}})_{\text{net}} = 0 \text{ J}$